## 1 Introduction

## Advantages of ideal imaging FTS's:

- Spectral resolution can be varied easily by changing mirror scan path length and is usually much better than for a similar size dispersive instrument.

  High light throughput leads to improved signal to detector background ratio.
- background ratio.

  Because the radiance spectrum is real the interferogram is an even function which allows using only one-sided interferograms, thus reducing the data storage requirements.

  2-d image of scene is acquired allowing analysis of moving objects in the scene.

#### Problems of ideal imaging FTS's:

- Larger photon background noise because all light from a spectral region falls on the detector.
- Large dynamic range requires a large number of digitization levels.

- Problems with real imaging FTS data:

   Lenses, filters and beam splitter (sometimes also electronic amplifiers) introduce phase errors due to frequency dependent path differences which result in a broadening of the center-burst. Because the center-burst of a FTS with phase errors is in general asymmetric, full two-sided interferograms need to taken. Dispersion also reduces the dynamic range thus requiring fewer quantization levels [Criffiths and de Haseth].

   Pointine little spaces out spatial information and can intro-
- and de Haseth].

  Pointing jitter smears out spatial information and can introduce unwanted spectral features.

  Internal reflections within the detector cause secondary ghosts (channeling) of the center-burst to appear in the spatial or interferogram domain

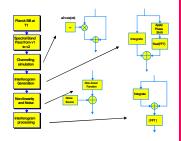
  Non-linear detector response causes harmonics to appear in the spectral domain

  Dand or point vivole must be corrected before jitter can be
- Dead or noisy pixels must be corrected before jitter can be removed.

- Phase corrections using complex FFT's reduce the broadening of the center-burst.
- or the center-burst.
   Correlation of flat-fielded frames of interferogram cube with a reference frame determines x/y shifts which can then be used to re-sample the image cube.
- Mask the channeling out before performing the Fast Fourier transform (FFT) to reduce the ringing.
- Correct the measured data by applying the inverse of the non-linear detector model to minimize spectral harmonics.
- non-mear detector model to minimize spectral harmonics.

  Use bad pixel detection algorithms and morphologic image operators to interpolate values over bad pixels.

#### A flexible FTS model



- <u>Parameters for simulation:</u>
   3 calibration sources at temperatures  $T_0 = 20C, T_1 = 20C, T_2 = 20C, T_3 = 20C, T_4 = 20C, signal to noise ratio <math>SNR = 1000$ , numbe samples  $N_f = 4096$  frames, and a responsivity between and  $1250 \ cm^{-1}$ .
- Phase dispersion model:  $\phi(\nu) = 500(\frac{\nu}{\nu_{max}})[1 + 0.3(\frac{\nu}{\nu_{max}})^2]$
- Channeling amplitude:  $amplitude(\nu) = (1. + 0.2 \cos(\omega_0 \nu))$
- Nonlinear model:  $DN[nonlin] = DN[lin]^d$  where d = 0.33 Task. Simulate the effect of phase errors, channeling and nonlinearity on the 2-point calibration error on the measured black body  $(BB_1)$  using  $(BB_9)$  and  $(BB_2)$  measurements.

## 2.1 Two-point calibration

Let  $I_k(x,i,j)$  be the interferogram of the k-th calibration source at  $T_k$ . Let's define the measured spectral response (MSR) at the

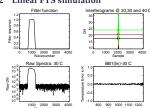
$$MSR_k(\nu,i,j) = \big| FFT[I(x,i,j)] \big|$$

. Given Planck's function B(), the calculated BB radiance for  $T_k$  is  $CBB_k(\nu)=B[\nu,T_k]$ . Assuming a linear detector the calibrated radiance  $L_1(\nu)$  of  $BB_1$  is:

$$L_1(\nu) = \frac{MSR_1 - a(\nu, i, j)}{h(\nu, i, j)}$$

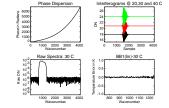
$$a(\nu, i, j) = MSR_0(\nu, i, j) + b(\nu, i, j)CBB_0(\nu), \text{ and}$$
  
$$b(\nu, i, j) = \frac{MSR_2(\nu, i, j) - MSR_0(\nu, i, j)}{CBB_0(\nu) - CBB_0(\nu)}.$$

### 2.2 Linear FTS simulation



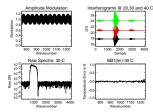
The strongly peaked symmetric center-burst which al-

## 2.3 Linear + dispersion FTS simulation



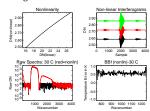
Note: The spread-out center-burst is no longer symmetric anymore, thus two-sided interferograms need to be taken. Also the dynamic range is reduced compared to the non-dispersed FTS.

#### Linear + dispersion + channeling FTS simulation



Note: Channeling causes ghosts of the center-burst. In the spectral domain the channeling manifests itself as amplitude modulations.

# Non-linear + dispersion + channel-ing FTS simulation



Note: The spectral harmonics occur at the sum and differences of the in-band wavenumbers. There is a corresponding nonzero mean temperature offset on BB, and increased temperature noise compared to linear FTS's.

#### Radiometric corrections

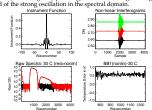
#### Phase error correction

ept: Using a phase estimation technique it is possible to ert a dispersed interferogram into a non-dispersed inter-

Note: Experience with FTS data shows that there is usually only a small improvement of SNR (theoretical improvement is  $\sqrt{2}$ ) if a phase correction is performed.

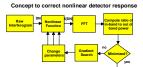
### 3.2 Channeling effect correction

Concept: Cutting off (apodizing) of the channeling bursts gets rid of the strong oscillation in the spectral domain.



Note: Removing channeling eliminates the sinusoidal modu-lation in the spectral domain. Removing the channeling, how-ever, introduces instrument functions with side lobes (see fig-ure) which introduce ringing near narrow spectral features, i.e. atmospheric absorption lines.

## 3.3 Non-linear response correction



Retrieval of the exponent d uses the ratio

$$R = \frac{max\{in-band\ Signal\}}{\sigma\{Oul-of-band\ Signal\}}$$
 Retrieval of Ni, parameter

Note: The exponent 0.33 was correctly identified

# Geometric corrections

Problem: Given a reference image I(0) and a sequence o x/y shifted and rotated images find the optimal shifts,  $x_{op}$  and  $y_{opt}(n)$  and rotation,  $\phi_{opt}(n)$ , to minimize:

 $RMSE(I(0) = rotate(shift(I(n)), x_{opt}(n), y_{opt}(n)), \phi_{opt}(n))).$ 

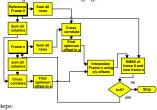
#### Possible Algorithms

- 1. Direct 3-D cross correlation to find x/y shifts and rotation.
- 2. Direct 2-D cross correlation to find x/v shifts
- Adaptive (from low resolution to high-resolution) 2-D image correlation
- 4. Reduce problem to separable 1-D correlations to also han-

Advantages of 4 over 1-3: Perform simple 1-D correlations rather than computationally expensive 2 or 3-dimensional. Methods 2 and 3 only work for shifts.

## 4.1 Fast x/y shift determination

Block diagram for a fast tracking algorithm:



- 1. Initialize a maximum search range R<sub>0</sub>, e.g. +/- 5 pixels
- 2. Sum over all rows and columns of reference frame to obtain 1-D vectors  $S_z(0) = \sum_z (I(0))$  and  $S_y(0) \sum_u (I(0))$ .
- 3. For frame n and k iterations do:
  (a) Let  $x_{opt,n}(n) = x_{opt}(n-1)$  and  $y_{opt,n}(n) = y_{opt}(n-1)$ (b) Cross-correlate 1-D vectors over a range of shifts from -R to R in  $\Pi$  steps:

$$\begin{split} S_x(n) &= \sum_x (shift(I(n), x_{opt}(n-1), y_{opt}(n-1))), \text{ and} \\ S_y(n) &= \sum (shift(I(n), x_{opt}(n-1), y_{opt}(n-1))) \end{split}$$

with  $S_x(0)$  and  $S_y(0)$  to find residual shifts  $\delta_x$  and  $\delta_y$  which minimize  $RMSE(S_x(0) = shift(S_x(n), \delta_x, \delta_y))$  and  $RMSE(S_y(0) = shift(S_y(n), \delta_x, \delta_y))$ . (c) Let  $x_{xy,k}(n) = x_{xy,k-1}(n) = \delta_{x,k-1}$  and  $y_{xy,k-1}(n) = y_{xy,k-1}(n) = \delta_{y,k-1}$ .

(d) Reduce the range by  $R_k = R_{k-1}/2$ 

#### 4.2 Fast rotation determination

- 1. Initialize a maximum search angle range for Φ<sub>0</sub>, e.g. +/- 5
- 2. Sum over all rows and columns of reference frame to obtain 1-D vectors  $S_z(0) = \sum_z [I(0)]$  and  $S_y(0) \sum_u (I(0))$ .
- 3. For frame n and k iterations do:
- (a) Let φ<sub>opt</sub> u(n) = φ<sub>opt</sub>(n 1)
   (b) Cross-correlate 1-D vectors over a range of angles from -Φ to Φ in 11 steps:

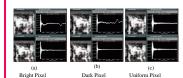
$$\begin{split} S_x(n) &= \sum_x (rotate(I(n),\phi_{opt}(n-1))), \ \text{ and} \\ S_y(n) &= \sum (rotate(I(n),\phi_{opt}(n-1))) \end{split}$$

with  $S_x(0)$  and  $S_y(0)$  to find residual rotation angle  $\delta\phi$  which minimize  $RMSE(S_x(0)-rotate(S_x(n),\delta\phi).$  (c) Let  $\phi_{op,k}(n)=\phi_{op,k-1}(n)-\delta\phi_{k-1}$  (d) Reduce the angular range by  $\Phi_k=\Phi_{k-1}/2$ 

#### 4.3 Effect of jitter

#### Effect of jitter depends on the surrounding area

- A bright pixel surrounded by dark pixels shows strong base line shifts
- A dark pixel surrounded by dark pixels shows strong base line shifts
- A pixel in a uniform region shows no baseline shifts Effect of Jitter Restoration on Pixels near Contrasts (a,b) and in uniform Regions (c) shown in the FTIR data cube



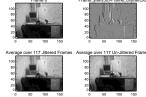
- La Generate a simulated linear FTS image cube  $C_0$  and jitter each frame of the cube using a known jitter function  $x_{off}(n)$  and  $y_{off}(n)$  to obtain a cube  $C_j$ .
- Perform un-jittering of cube and store result in C<sub>w</sub>
- 3. Fourier transform  $C_0$ ,  $C_j$  and  $C_u$  and compute the average spectra over a region of 32 x 32 pixels



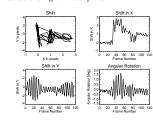
Notes: The un-jittering process has little effect on the spec tral region of interest (500-800 arbitrary wavenumbers) but re-duces the spurious signal near zero wavenumber.

## 4.4 Results

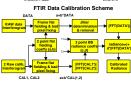
Experiment 1: Recorded 117 frames of video from camera placed on a shaking surface and tracked shifts and rotations Effect of jitter and jitter-correction on overall image quality:



Results of tracking for video sequence:



# Experiment 2: Track motions in a simulated FTS cube



Additional processing: Frame flat fielding: There may be residual stripes in each frame for the CAL and DATA cubes which need to be removed before cross-correlations are performed for jitter removal

#### Bad pixel fixing steps:

- 1. Find "bad pixels"="dead" pixels and "noisy" pixels
- 2. Grow a region around "bad pixels" using a cross shaped kernel
- 3. Delauney triangulation of neighbor pixels and quintic in-terpolation at bad pixels

#### 5 Data compression

- Only a fraction (1/8 th) of the spectral image cube is retained after the FFT which is a  $N\log N$  complex operation.

Example: Compute ratio of the number of multiplications required for a reduced FFT with down-sampling over the number required for a full FFT a function of interferogram length N and finite-impulse-response (FIR) length L:

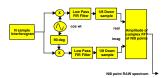
$$R = \frac{N/8 \log_2 N/8 + 2N/8L}{N \log_2 N}$$



roblem: Find a solution to reduce the amount of operations generate the spectral cube and save storage space for the

lution: Modulate the interferogram and low-pass filter with a super-heterodyne receiver.

# Down Sampling of FTIR Data to 1/8 of Original Number of Samples



# Conclusions

Several "real world" effects on FTS data have been presented and some methods to reduce their effect:

- Channeling can be removed by apodizing the interferogram with the penalty of introducing ringing near spectral lines or calibrated out given a sufficiently stable FTS system.
- Jitter removal improves image sharpness but has little effect on spectral fidelity if the jitter is low-frequency.
- Non-linearity corrections eliminate systematic calibration errors.
- Super-Heterodyne processing reduces the amount of operations to generate the spectral cube and storage requirements.

# 7 References

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- A very nice introduction in French to Michelson inter-ferometers can be found at: http://www.sciences.univnantes.fr/physique/enseignement/tp/michelson/michp.html
- A nice write-up by Paul Van Delst on correcting HgCdT non-linearities for the AERI instrument can be found at: http://airs2.ssec.wisc.edu/~paulv/aeri/aerinsa.nlanalysis/971113b1/971113b1.html
- Software to perform jitter correction using a hierarchical cross-correlation technique can be found at: http://idlastro.gsfc.nasa.gov/ftp/contrib/varosi/vlib/
- The PostScript version of this poster will be available on: http://nis-www.lanl.gov/~borel